

# High brightness and high average current electron sources and their applications

APT seminars, FermiLab

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Northern Illinois University

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- 1 Introduction
- 2 Field Emission cathodes at NIU
- 3 Electron source at IARC, FermiLab
- 4 LCLS-II HE injector
- 5 Conclusion

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# Acknowledgment



I would like to acknowledge the work and help I received from these people of whom without, this work would not be possible.

*From NIU:* P. Piot, D. Mihalcea, T. Xu, A. Lueangaramwong, S. Valluri, N. Tom, N. Adams. A. McKeown, V. Korampally, I. Salehinia,

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*From SLAC:* Cho-Kuen Ng, Liling Xiao, Lixin Ge

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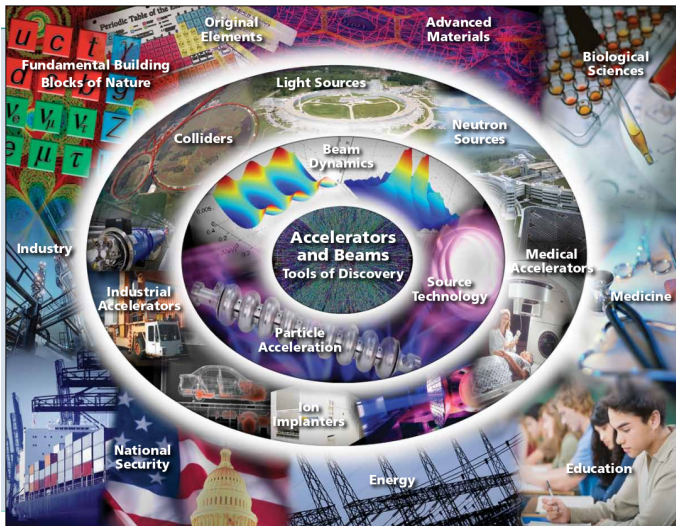




# Motivation



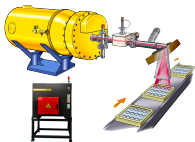
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# Electron beams



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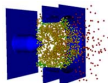


Food irradiation

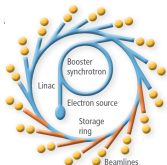
[1]



electron ion collider

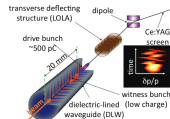


generation of electron beams from nano-tips  
<https://www.niu.edu/advanced-accelerator-randd>



accelerator based light sources

<https://simple.wikipedia.org/wiki/Synchrotron>



[2]

Advanced Accelerator concept

\* †

\* <https://www.aerial-crt.com/>

† <https://www.bnl.gov/eic/>

# Motivation: high brightness electron beams



*Brightness* is related to the amount of charge in phase-space volume.

$$\mathcal{B} \sim \frac{q}{\epsilon_{\perp}^2 \epsilon_{\parallel}}$$

Generation of electron beams using  
photo-emission followed by acceleration  
in radio-frequency structure

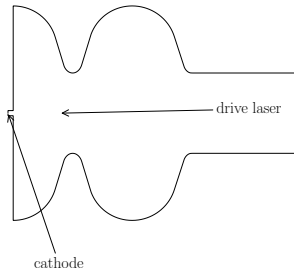


photo emission in RF structure [3]

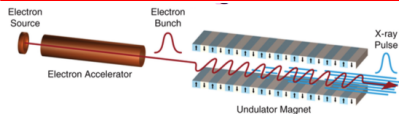
- The emission is guided by a laser trigger.
- To a first approximation, the emitted particle distribution represents the initial laser pulse.
- Characterised by  $QE \sim \frac{\Delta Q/q}{\Delta E/\hbar\omega}$  [4]

# Application: brightness



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## Future Free Electron lasers



$$\rho \sim (\mathcal{B})^{1/3}$$

$$\epsilon_n \lesssim \gamma \beta \frac{\lambda}{4\pi}$$

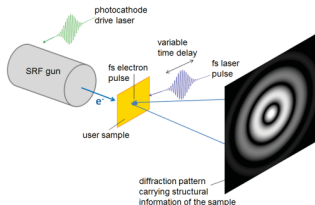
This  $\rho$  parameter controls the exponential gain length  $L_g \sim \rho^{-1}$  and the FEL wavelength  $\lambda$  is set by the electron beam emittance and energy [5, 6].

$$Q \sim 100 \text{ spC}, \sigma_t \sim 1 \text{ ps}, \epsilon_x \sim 100 \text{ nm}$$

<sup>‡</sup><http://web.stanford.edu>

‡

## Ultra fast electron experiments



Ultra-Fast electron diffraction setup [7]

Foot-prints accelerator that can provide:

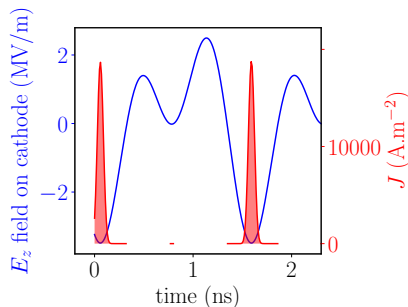
$$Q \sim 10 \text{ sfC}, \sigma_t \sim 100 \text{ fs}, \epsilon_x \sim 1 \text{ nm}$$

[8][9].



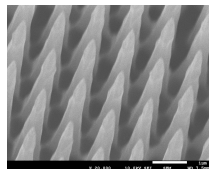
# Motivation: High average current

Generation of electron beams using  
Field Emission (FE) cathodes:



$$j = A(\phi)[\beta_e E]^2 e^{\frac{-B(\phi)}{\beta_e E}} [10] \quad (1)$$

where  $\phi$  is the work function,  $E$  is the electric field,  $\beta_e$  is the field-enhancement factor and  $A(\phi)$ ,  $B(\phi)$  are constants.



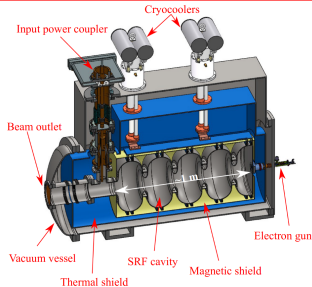
An array of Si nano tips

- Array of nano-tips can be used to enhance the field at the surface
- The emission is solely guided by the applied electric field
- Depends on electric field amplitude and the material

# Application: high-average power



## High average-power beams



conceptual design of 4.5 cell gun cooled by 2 cryocoolers

The complex infrastructure associated SRF technology is a challenge in applying it outside of research facilities. (e.g. liquefaction and storing of Helium). Recent work in conduction cooling can be the solution [11, 12]

$$P = Q \times f \times \varepsilon \quad (2)$$

- Many industrial applications require few MeV electron beam with high average power (100s kW) [13, 14].
- Conduction-Cooled SRF systems can provide cooling for up to 4 K.
- Field Emission is an excellent candidate because of its self-gating mechanism and high repetition rate.
- The elimination of the use of a laser-trigger system simplifies the setup a lot.
- When compared to Thermionic Emission, FE makes the SRF-cathode coupling much simpler since it is cold and it does not require insulation
- No back bombardment as in the case of Thermionic.

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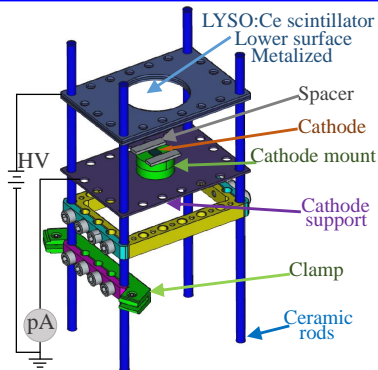
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# FE cathodes at NIU



To test FE cathodes, a DC test stand was designed and built at NIU.

- A simple diode configuration setup.
- High voltage applied at the anode.
- Different spacer can be used.
- Scintillating screens with a CCD camera to measure the beam distribution.
- Ultra-high vacuum chamber.
- In-house control system to control and monitor the setup



schematic view of the setup courtesy of [15]

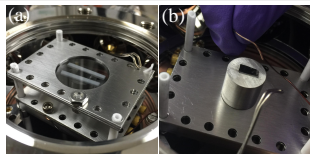


# Results I

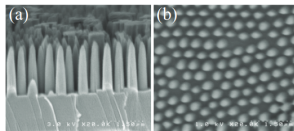


- Cathodes were made by our collaborators at NIU and ANL.
- Different cathodes were made and tested
- Emission from sharp edges around the cathode (dark current)

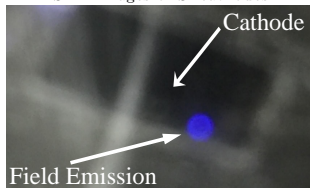
Self-assembled monolayers of Silica spheres deposited on the Si wafer. The spheres form a mask to structure the wafer via etching processes. A first anisotropic profile is performed with chlorine. A reactive-ion etching process is then achieved using an Ar/SF<sub>6</sub> composition of gases to create an isotropic etch profile. Finally, the silicon tips are formed via thermal oxidation;



setup at NIU



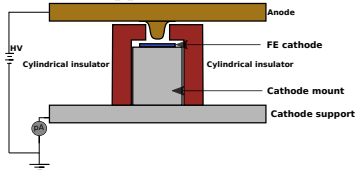
SEM images of Si cathodes



Emission observed from the edges of the cathode

## Results II

New spacer and anodes were designed to suppress emission



Schematic views of the modified setup to suppress emission from undesired regions.

F-N current is more explicitly given by:  
[16]

$$j = A(\phi) [\beta_e E]^2 e^{\frac{-B(\phi)}{\beta_e E}} \quad (3)$$

$$I = A a \phi^{-1} 10^{4.52} \sqrt{\phi} \beta^2 E^2 e^{\frac{-k\phi \frac{3}{2}}{\beta \times E}} \quad (4)$$

where  $a, k$  are constants,  $A$  ( $\text{m}^2$ ) is the effective emission area.

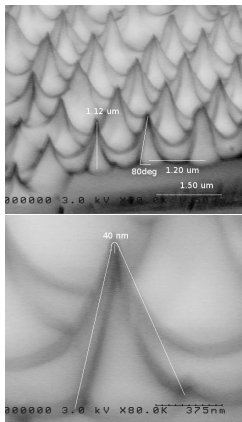
The common analysis for F-N behaviour is to plot the experimental data in a semi-log plot between  $\ln \frac{I}{E^2}$  and  $1/E$

$$\frac{\ln \frac{I}{E^2}}{1/E} = \ln(\xi A) - \frac{k\phi \frac{3}{2}}{\beta} \quad (5)$$

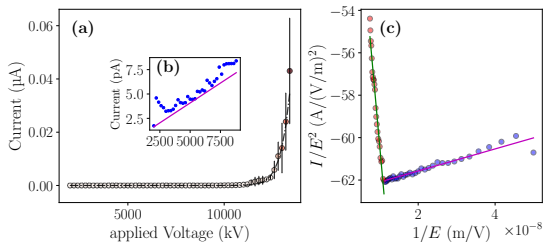
$\beta$ : is the field enhancement factor (ratio between how much the field is enhanced due to geometry compared to when it is flat)

# Results III

First cathode we successfully tested was Si



inverted SEM images of the cathode



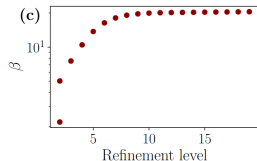
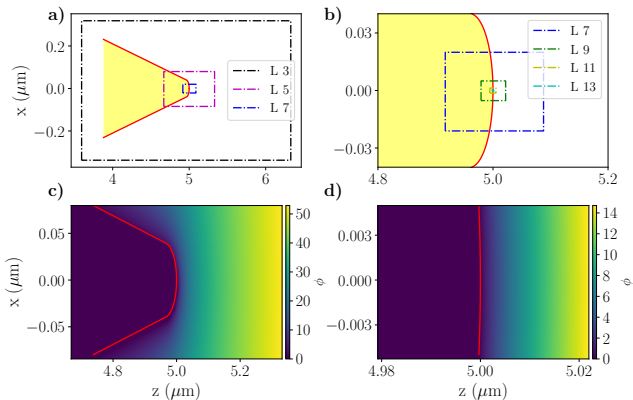
The calculated emitting area  $A_e$  and  $\beta$  were low but within our expected values.

$$\beta \sim 30$$

# benchmarking $\beta$



We use Particle-in-Cell (PIC) code WARP to simulate the geometrical effects of these nano-tips. It could gives us an idea what to expect and we can communicate with the engineering departments on our needs so they can deliver.



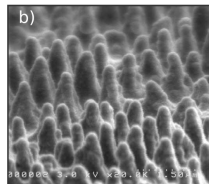
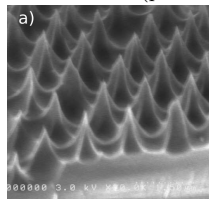
- 20 mesh refinement patches to resolve nm features of the tip
- Final  $\beta$  agrees with what we measured in the lab.

## UNCD results (FEA)



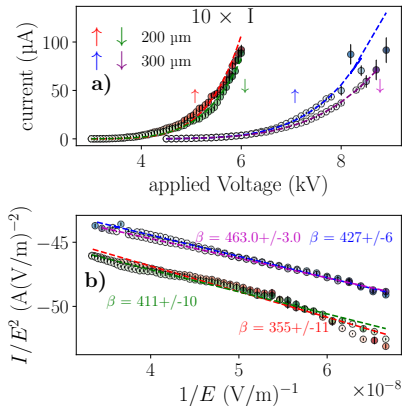
Several Si Cathodes were coated with Ultrananocrystalline diamond (UNCD) to test their performances and compare with Si cathode and planar UNCD cathodes (p-UNCD).

- $\beta$  is attributed to geometrical factors. However, grain boundaries may contribute to higher  $\beta$
- UNCD has previously shown lower turn on fields and more stable emission when compared to pure Si



before and after coating with UNCD

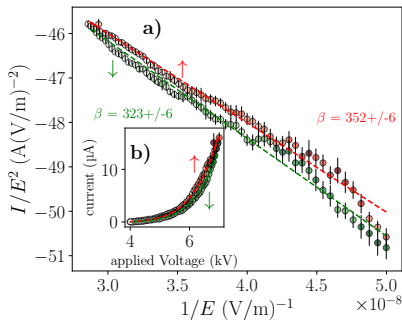
# UNCD-results



I-V characteristic curve (a) and F-N plot (b)

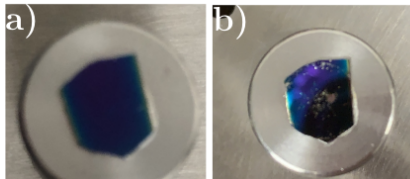
- The  $\uparrow$  and the  $\downarrow$  indicates whether the voltage was increasing or decreasing
- Different spacing were considered (200  $\mu m$  and 300  $\mu m$ )
- The current increased by an order of magnitude when the gap spacing was raised from (200  $\mu m$  to 300  $\mu m$ ) (data for 200  $\mu m$  was taken first)

## p-UNCD



I-V characteristic curve (b) and F-N plot (a)

- Planar-UNCD cathode was also tested
- The test was carried out only 200  $\mu\text{m}$ ) because the cathode was damaged



before

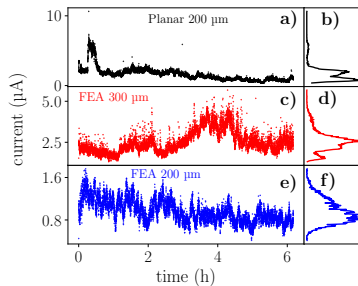
after

# Summary



**Table:**  $\beta$  and  $A_e$  for FEA and planar cathodes.

sample	spacing ( $\mu\text{m}$ )	$\beta$	$A_e$ $10^{-16} \text{ (m}^2\text{)}$
Si $\uparrow$	100	$27 \pm 2$	$1.2 \pm 0.5$
FEA $\uparrow$	200	$355 \pm 11 \pm 109$	$1.6 \pm 0.5 \pm 0.72$
FEA $\downarrow$	200	$411 \pm 10 \pm 126$	$0.31 \pm 0.065 \pm 0.12$
FEA $\uparrow$	300	$427 \pm 6 \pm 131$	$3.2 \pm 0.42 \pm 1.1$
FEA $\downarrow$	300	$463 \pm 3 \pm 142$	$1.3 \pm 0.07 \pm 0.4$
planar $\uparrow$	200	$352 \pm 6 \pm 108$	$0.56 \pm 0.09 \pm 0.19$
planar $\downarrow$	200	$323 \pm 6 \pm 99$	$0.96 \pm 0.16 \pm 0.34$



- Higher current for the 300  $\mu\text{m}$  for FEA
- Higher emission area between planar and FEA are purely geometric
- For the same spacing,  $\beta$  is very similar. Comparing with previous bare Si, this indicates that the source of  $\beta$  is mainly due to grain boundaries rather geometric features.



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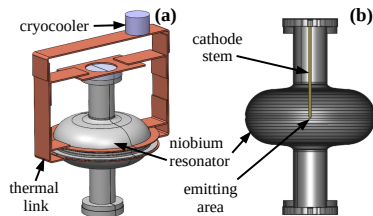
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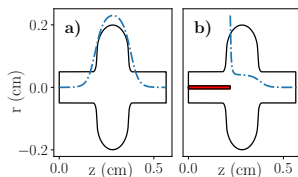
# Conduction cooled electron source

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- Based on an elliptical 650-MHz superconducting resonator.
- The cavity is cooled using conduction cooling instead of liquid He.
- Thermal links are made from high purity Aluminium.
- Cylindrical rod is inserted into the cavity
- The rod shifts the eigenmode of the cavity and enhances the field around it (just like a nano tip)



schematic view of the setup

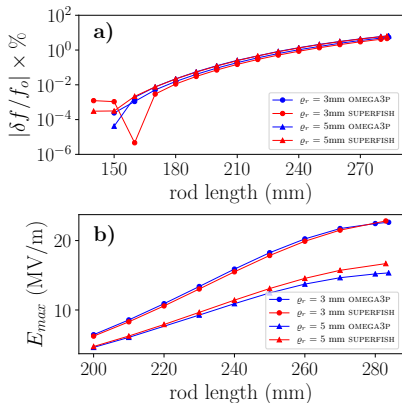


geometry of the nominal and modified cavity

# E-source at IARC



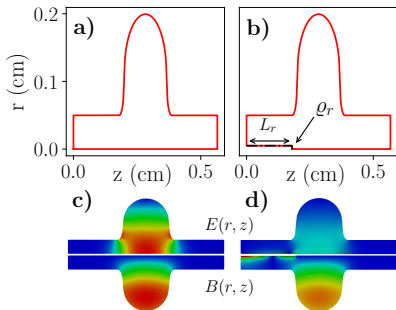
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shift in the frequency and peak axial electric field  
 $E_z(r=0)$  for different  $L_r$  and  $\rho_r$

- The system is cooled down to cryogenic temperatures by conduction cooling rather than the use of cryogenic fluids.
- Cryocooling capacity ranging from 1 - 2 W at  $\sim 4$  K
- Different rod lengths  $L_r$  and radius  $\rho_r$  were studied
- The field reaches its maximum when the rod is at  $L/2$
- Experiential constraints (cryocooler and LLRF) had to be met, so a moderate case of  $L_r = 22.0$  cm and  $\rho_r = 0.5$  was chosen

# Dissipated Power



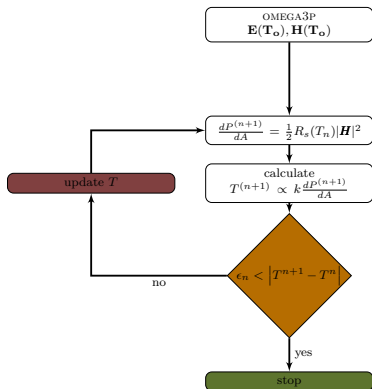
Electric and magnetic field for the nominal and modified cavity

$$\frac{dP}{ds} = \frac{R_s}{2} |\mathbf{H}_{\parallel}|^2$$

$$P = \frac{R_s}{2} \int ds |\mathbf{H}_{\parallel}|^2$$

- The change in the eigen modes introduces higher magnetic flux near the rod and flange.
- In order to make sure that the system stays below critical temperature of Nb, we did thermal analysis of the system on collaboration with the engineering department.
- The thermal model was coupled to the RF simulation via ANSYS

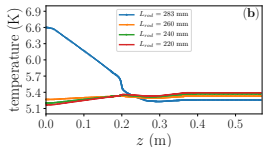
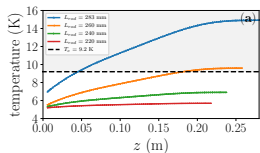
# Thermal Analysis



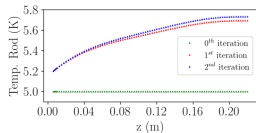
Computational loop for thermal calculations

- Electric and Magnetic fields are calculated based on surface resistance  $R_s$  of Nb at 5.0 K using OMEGA3P
- Dissipated power is calculated based on the magnetic fields and normalized to 1.6 Watt (determined by the cry cooler)
- Temperature profile  $T^{n+1}$  is calculated based on the given  $dp/ds$  using ANSYS
- If the difference between initial temperature  $T^n$  and  $T^{n+1}$  is small [ $\epsilon_n \sim \mathcal{O}(10^{-2})$ ] convergence is reached.

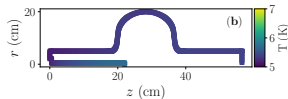
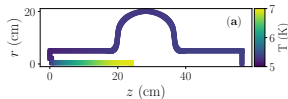
# Thermal Analysis II



Steady-state temperature reached for various value of rod length  $L_r$  along the rod (a) and external cavity wall (b).



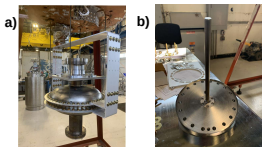
Temperature on the rod vs iteration



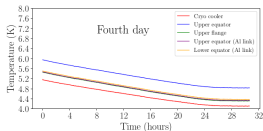
final temperature along the cavity for (a)  $L_r = 24.0$  cm and (b)  $L_r = 22.0$  cm

- Convergence is reached usually after 2 or 3 iterations.
- For cases where  $L_r > 24.0$  cm, temperature exceeded  $T_c$
- Highest temperature is at the rod's extremity.

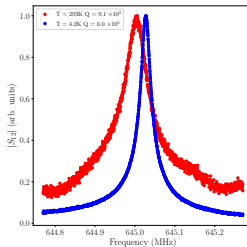
# Experimental work I



cavity with conduction cooled links (a) and rod with flange (b)

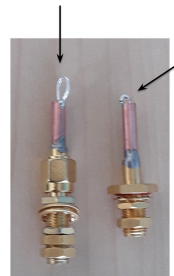


cooling rate vs time (showing only 4th day)



Measured  $S_{12}$  before and after cooling

- The setup was assembled and successfully cooled down
- Frequency measured is as expected  $\pm 2$  MHz.
- We designed RF coupler with  $Q_{ext} \sim 10^8$  to match the expected  $Q_o$ .



# Experimental work II



**Table:** Temperature comparison between the 2 cool downs

Location	Temp. run I (K)	Temp. run II (K)
Cryocooler port	4.1	4.1
Upper flange	4.8	7.3
Upper Equator	5.0	5.2
Lower Flange	6.9	8.2

$$E_{acc} = \sqrt{Q_2 P_t \left( \frac{R/Q}{L} \right)} [17]$$

$$R/Q = 155.7 \Omega$$

- There is a significant temperature difference on the flange (upper mostly)
- During the second cooling, we were able to do RF measurements
- The measured  $Q_o \sim 8 \times 10^6 \pm 10^3$  (Expected:  $Q_o \sim 10^8$ )
- Because the cavity  $Q_o$  was lower than anticipated, the  $Q_{ext}$  was much higher, this meant we are under-coupled (Forwarded power is mostly reflected and not stored in the cavity).
- The measured  $E_{acc} \sim \mathcal{O}(10^{-2}) \text{ MV/m}$  (Expected:  $E_{acc} \sim 1 \text{ MV/m}$ )
- The issue seems to be the thermal link connection between the thermal links and the upper flange.
- Possible contamination could increase the resistance

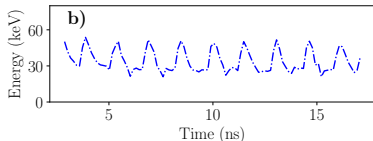
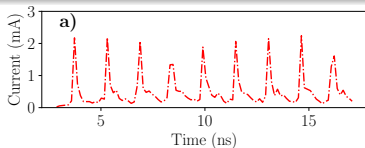


# Future work

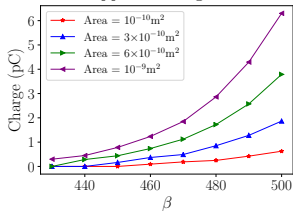


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- We are currently warming the cavity and getting ready to do another test before the Holiday.
- a UNCD cathode can be "glued" to the rod extremity.
- WARP was used to simulate emitted current based on previous results.
- Electrons are emitted using F-N equation
- a solenoid can be used at the exist control the beam size
- MHz repetition rate bunches can provide high average power for several applications.

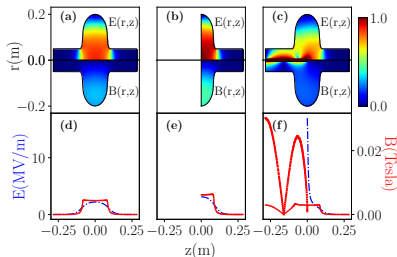


Current and final energy expected to see at the opposite flange



Charge extracted via FE for  $L_r = 22.0 \text{ cm}$

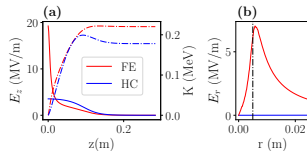
# High-brightness application



Difference between Full (a) half-model (HC) (b) and rod model (FE) (c)

**Table:** RF parameters simulated for the three cavity configurations under considerations.

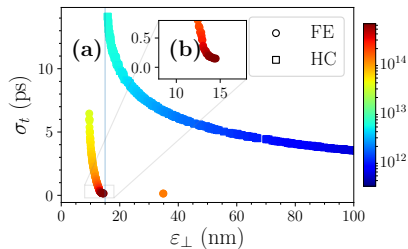
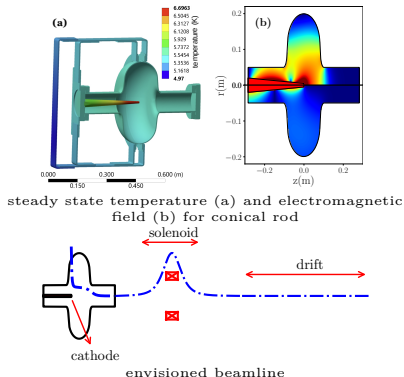
parameter	unit	FC	HC	FE
$f$	MHz	650	650	607
$E_z(r=0)$	MV/m	2.2	3.1	16.9
$Q$	—	$3.12 \times 10^8$	$3.12 \times 10^8$	$1.8 \times 10^8$



Energy gain (a) and radial field  $E_r(r)$  for HC and FE model

- Extending the rod to the center of the cavity gives the maximum  $E_z$  for acceleration.
- Comparing to a typical Half cell (HC) geometry from the same cavity the field is x4 times higher
- To keep the cavity under  $T_c$  the geometry of the rod needed to change.

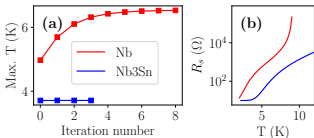
# High-brightness application



Pareto-Front from the multi-objective optimisation

- Changing the geometry of the rod from a cylindrical to a conical shape help reduce the  $dp/ds$  near the flange, which helps in maintaining the cavity under  $T_c$
- Using multi-objective optimisation coupled with beam-dynamics codes IMPACT-T we were able to minimize  $\sigma_t$  and  $\epsilon_x$

# Summary



- In terms of beam-dynamics and EM simulations, the model generate ultra-fast electron bunches with superior transverse brightness than typically achieved in a standard half-cell configuration based on a similar elliptical geometry.

- Proof of principle tests are still going and hopefully we will be done before the end of the year.
- The same principle can be applied to an N cells to produce higher energy.
- Using photo-emission to produce low emittance beams and short bunched beams.
- The system can be operated for different cathode configuration to produce electron beams for different applications
- Reducing surface resistance  $R_s$  by coating with Nb<sub>3</sub>Sn could increase the electric field.

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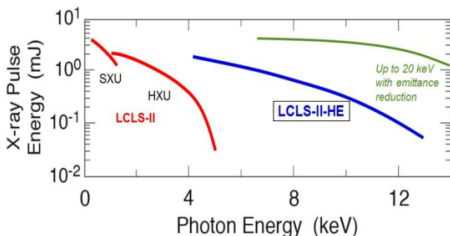


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# LCLS-II HE: overview



expected increase in photon energy with emittance reduction for LCLS-II HE [18]

	LCLS-II	LCLS-II HE
electron energy (GeV)	4	8
photon energy (keV)	5	13-20

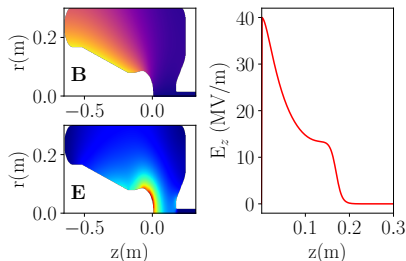
**Table:** Expected performance for LCLS-II and LCLS-II HE

- The LCLS-II HE is an upgrade to the LCLS-II. It will increase the beam energy up to 8 GeV and photon spectral range up to 12.8 KeV.
- The spectral range can be improved by reducing the emittance of the beam (up to 20 KeV).

**Table:** Required bunch parameters for the injector of LCLS-II HE

Parameter	Value
Bunch charge	100 pC
$\epsilon_x$	$\leq 0.1 \mu\text{m}$
$\sigma_z$	$\leq 1 \text{ mm}$
KE ( 8 cav)	$\geq 90 \text{ MeV}$
$\sigma_p$	$\leq 200 \text{ keV}$
$\sigma_p$ (unc)	$\geq 5 \text{ keV}$

# LCLS-II HE injector modeling



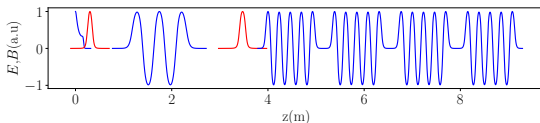
Field map of ANL proposed design (ANL ori) for LCLS-II injector [19]

**Table:** RC cavity parameters

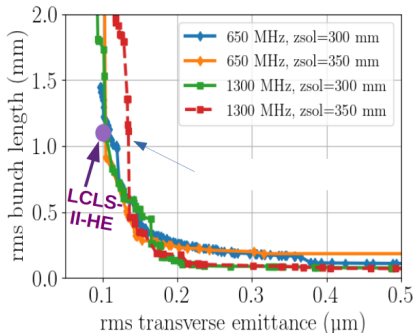
Parameter	Value
$f_o$	127 MHz
$E_{cathode}$	40 MV/m

- The design is based on superconducting reentrant-cavity (RC) geometry rather than elliptical  $N + 1/2$  gun.
- RC can support sub-GHz frequencies with a reasonable sized cavity.
- Lower frequency operation is beneficial as it relaxes the helium-temperature requirements (e.g. operation at 4.2K is possible instead of 2.7K) ( $R_s \sim f^2$ )
- Beam dynamics simulation with multi-objective optimisation using ASTRA

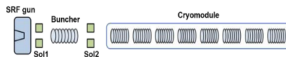
# example of optimisation



Electric and Magnetic fields along the injector.



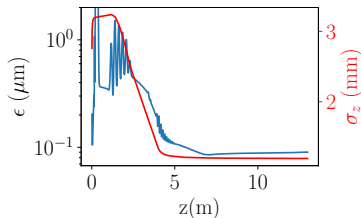
Pareto-Front associated with optimisation of  $\sigma_z$  and  $\epsilon_x$  for different cases



- Initial design was obtained and currently we are working to improve it.
- Different cases for the cavity were simulated using OMEGA3P
- Beam dynamics simulation with multi-objective optimisation using ASTRA



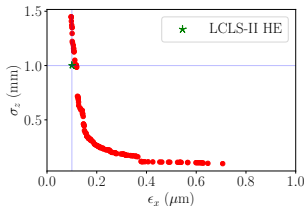
# Optimum Solution: example



Evolution of  $\sigma_z$  and  $\epsilon_x$  downstream the injector

**Table:** Simulation result

Parameter	Value
$\epsilon_x$	0.09 $\mu\text{m rad}$
EK	45.958 MeV
$\sigma_z$	1.2 mm
$\delta_p^*$	9.7 KeV



best solution so far was obtained with a 650 MHz buncher and a solenoid as close as possible to the gun (300mm)

- The current design almost meets the LCLS-II HE requirements (for 100 pC,  $\sigma_z < 1\text{mm}$  and  $\epsilon_x < 0.1 \mu\text{m}$ )
- More improvement can be made in focusing solenoid and in the geometry of the cavity
- So far, ellipsoidal initial bunches have been considered.
- Thermal emittance is a big factor in these simulations

# Emittance contribution



In photo-injector, (assuming uncorrelated) the emittance can be the sum of different contributions including:

$$\epsilon_n \propto \sqrt{\epsilon_{th}^2 + \epsilon_{rf}^2 + \epsilon_{sc}^2 + \epsilon_{chrom}^2 + \epsilon_{geom}^2} [20]$$

$$\epsilon_{th} = \sigma_x \sqrt{\frac{MTE}{mc^2}}$$

$$\epsilon_{sc} \propto \frac{I}{\alpha} \mu(A), \text{ where } \alpha = \frac{eE_o k}{2mc^2}$$

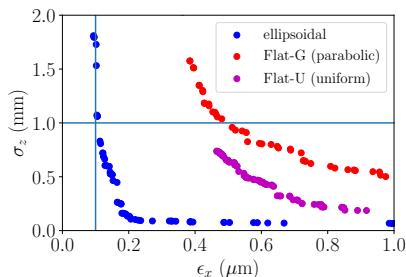
$$\epsilon_{chrom} = \sigma_x^2 \frac{\sigma_p}{mc} K |\sin KL + KL \cos KL|$$

- Thermal emittance is related to the mean transverse energy (MTE) and the laser spot size.
- Minimize the space charge contribution by increase  $E_o$  and laser shaping
- minimize the beam size just before the solenoid to reduce Chromatic aberration

## More studies: laser pulse



So far in the previous studies, we only considered a uniformly filled ellipsoidal bunch. We are also considering other distribution



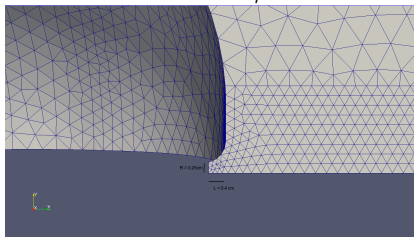
Pareto-Front associated with optimisation with different laser shapes

- Space charge force linearization in ellipsoidal electron bunches can reduce the emittance [21].
- experimental constraints can limit this laser pulse
- Flat-U: plateau distribution in time with a transversely uniform distribution (disk) (cylinder bunch)
- Flat-G: plateau distribution in time with the parabolic transverse radial distribution

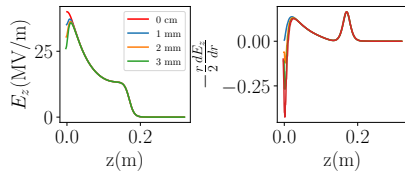
# More studies: aberration



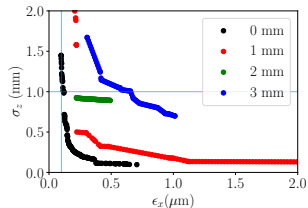
In order to try to see minimize the effect  $\epsilon_{chrom}$ , we tried to retract the cathode to introduce  $E_r$ :



An example of cathode retraction



$E_z$  and  $E_r$  for different lengths ( $r=0.75\text{mm}$ )



Pareto-Front associated associated with different cathode retraction

- The contribution of the higher field gradient at the cathode is larger than focusing effect from the radial field.

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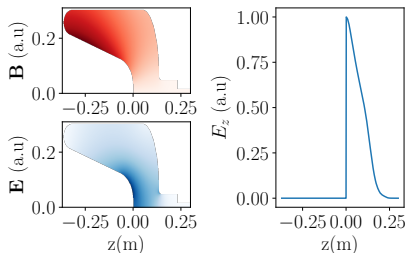
# Conclusion



- FE is a simple and appealing method of extracting electrons for high-average current applications.
- Emission uniformity and robustness of FEA is still an issue.
- The conduction-cooled source was designed and built. Comparing the 2 cooling attempts we had suggest we have an issue with some thermal connection. More attempt before the end of this year.
- In terms of beam-dynamics the conduction-cooled source with the enhanced field, produce brighter beams (order of magnitude) compared to similar geometries with the same dissipated power.
- Injector modeling for the LCLS-II HE is going. Optimisation to include the cavity geometry is undergoing.
- Expanding on the initial design would be to include the e-gun geometry in the optimisation process as well as laser pulse shaping.

# Questions?

# WIFEL gun



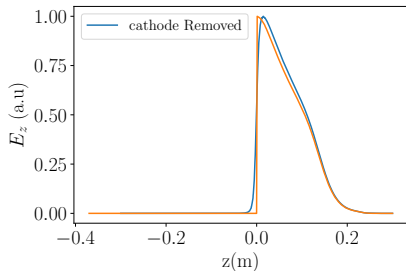
Associated  $E$  and  $B$  for the WIFEL gun



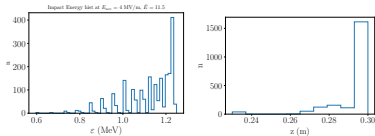
WifEL gun being unpacked at ANL

- Transported from SLAC to ANL (currently at ANL)
- can support a low-frequency (sub-GHz) fundamental mode with a reasonably-sized cavity
- Low-frequency operation is beneficial as it relaxes the helium-temperature requirements
- High repetition rate (sub MHz)
- The cavity was tested previously with  $E_z$  20 MV/m

# WiFEL gun



axial electric field  $E_z$  when the cathode is removed



- Currently, the gun is being tested for vacuum leaks.
- Cooling down operation is expected to start next month.
- Testing quality factor  $Q$  and  $V_{acc}$  is expected without the cathode.
- Dark current studies suggest that emitted electrons will not survive to the exist of the gun.
- X-ray and Gamma-ray detectors will be used to infer the photon energy to the electron energy.



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